

INSPECTION SERVICES FOR THE CITY AND CAMROSE COUNTY

PERMIT NO.		

	PRIVATE SEWAGE T	REATMENT SYS	TEM PERMIT	
Date:	Municipality		Roll #	Zone
Permit Applicant: ☐ Ow	vner Contractor			
Owner Name		Mailing Add	dress	
City	ProvinceF	Postal Code	P	Phone
Cell	Email			Fax
Contractor/Firm Name		Mailing Ado	dress	
City	ProvinceF	Postal Code	P	Phone
Cell	Email			Fax
Project Location Street/Rural A	ddress			
LotBlock	Plan	Section	Township	RangeW4
INSTALLATION DETAILS				-
TYPE OF OCCUPANCY	TYPE OF WORK	INSTALL	ATION	TREATMENT DISPOSAL METHODS
☐ Single Residential ☐ Commercial ☐ Industrial ☐ Offsite Manufactured Home ☐ Shop ☐ Accessory Building ☐ Other:	□ New □ Renovation □ Subdivision □ Other:	□ New □ Alteration Expected Volume or □ m³/day □ litres/day □ gallons/day (not to exceed 25 m³/day # of bedrooms: (residential including base development)	()	□ Septic Tank □ Holding Tank □ Treatment Mound □ Treatment Field □ Open (Surface) Discharge □ Packaged Sewage Treatment Plant □ At-Grade □ Privy □ Other:
protected under Part 2 of that Act and section 63 of and nature of the permit may be included on reports	the Safety Codes Act. It will be used for processing s provided to a municipality or made available to the	permit applications, issuing per he public as required or allowed	mits, safety codes complian d by legislation. Personal inf	edom of Information and Protection of Privacy Act and will be ce monitoring and verification. The name of the permit holder formation may also be used by the city of Camrose to conduct his application to the City of Camrose FOIPP Coordinator at
Certified Installer's Name (Print)	Certified Installer's Sigr	nature	—— н	lomeowner Signature (homeowner permit only)
Certified Installer's PS#				y signing this application I hereby certify that I own or rill own and occupy this dwelling.
	0	ffice Use Only		
Permit Fee	SCC Levy (\$4.50 or 4% of permit fee, max \$560.00)		Issuer's Name	
Travel Fee (Includes GST)	Total Cost		Issuer's Signature	2
Credit Card No.:	Receipt No.		Designation Num	nber
	Expiry:		Permit Issue Date	
	SCO Designation No.		SCO Signature	

Private Sewage Treatment System

The following information will be required when submitting an application for a private sewage treatment system permit.

Site plan

Location of all buildings/proposed buildings and improvements Location of well/cistern and any sloughs or waterways, water courses and property lines.

Septic tank, sewage holding tanks or sewage effluent tanks shall not be located within

- a) 10 m (33 ft.) of a water source or water well,
- b) 10 m (33 ft.) of a water course,
- c) 1 m (3.25 ft.) of property line, and
- d) 1 m (3.25 ft.) of a building

Open Discharge

- 1) An open discharge system may be installed in a location that provides separation distances from the point of discharge of not less than
 - a) 50 m (165 ft.) to a water source includes water well, and or cistern
 - b) 100 m (330 ft.) from a licensed municipal water well
 - c) 45 m (150 ft.) to a water course except as required by Article 2.1.2.4.
 - d) 90 m (300 ft.) to a property line, and
 - e) 45 m (150 ft.) to a building.
- 2) The effluent discharge piping shall be buried to at least the point where the separation distances set out in Sentence (1) are met.

Treatment Fields

- 1) A treatment field, measured from any part of a weeping lateral trench, shall not be located within
 - a) 15 m (50 ft.) of a water source or water well,
 - b) 100 m (330 ft.) of a licensed municipal water well,
 - c) 15 m (50 ft.) of a water course, except as provide in Article 2.1.2.4,
 - d) 1.5 (5 ft.) of a property line,
 - e) 10 m (33 ft.) from a basement, cellar, or crawl space, ¹
 - f) 1 m (3.25 ft.) of a building that has a permanent foundation but does not have a basement, cellar or crawl space, and
 - g) 5 m (17 ft.) from a septic tank or package sewage treatment plant.
 - ¹ Note: Clause (1)(d) The 10m (33 ft.) requirement to a basement, cellar, crawl space is intended to protect excavations below grade from accumulating migrating effluent. A crawl space that is not below grade, or where the level of the ground surface at the soil based treatment area is below the level of the crawl space the separation required is 5 m (17 ft.) clearance, as it can be treated as a building without a basement.

Treatment Mounds

- 1) A treatment mound shall not be located within
 - a) 15 m (50 ft.) of a water source or water well,
 - b) 100 m (330 ft.) from a licensed municipal water well
 - c) 15 m (50 ft.) of a water course, except as provided in Article 2.1.2.4.
 - d) 3 m (10 ft.) of a property line,
 - e) 3 m (10 ft.) of a septic tank,
 - f) 10 m (33 ft.) of a basement, cellar or crawl space, and
 - g) 10 m (33 ft.) of a building that does not have a basement, cellar, or crawl space.

Private Sewage System Design Document Example/Template Open Discharge

PREFACE

This is an example Design Document for a septic tank and open discharge system. It reflects the information needed to demonstrate the design considerations for the particular site and system required by the Private Sewage Standard of Practice 2009 (Standard) have been made. Considerations needed for a particular site may go beyond those used as an example in this document.

This example document can be used as a template by editing or adding critical information to suit the particular site and system.

While it is preferable to use a consistent format to facilitate quick review, other formats of the design document may be accepted by the Safety Codes Officer (SCO), if the document includes the required information that shows the necessary design considerations were made.

A design is required in support of a permit application. It includes drawings and supporting information as it applies to the specific design. This is the information a SCO will review to evaluate whether design considerations required by the Standard have been adequately made prior to issuing the permit.

Including this design in the operation and maintenance manual that must be provided to the owner, will simplify development of the operation and maintenance manual.

PRIVATE SEWAGE SYSTEM DESIGN EXAMPLE - OPEN DISCHARGE

Joe Smith Box 1, Somewhere, Alberta

Legal Description of Property:

NW Sec 31, Twp 36, Rge. 28, W of 4 Mer.

Lot 1; Blk 1; Plan 123450

19035 - Rge. Rd. 28

Municipal Address:

The sewage system includes a septic tank and open discharge system. This system is suitable for the site and soil conditions of this property. The design reflected in the following applies, and meets, the requirements of the current Alberta Private Sewage Systems Standard of Practice (Standard) to achieve effective treatment of the wastewater from this residence.

This sewage system serves a 4-bedroom single family dwelling. Based on the characteristics of the home identified during our review, the total peak wastewater flow that must be used for this design is 461 Imp. gallons per day. Although peak flow used in the design is 461 Imp. gal/day, an average operating flow of 300 lmp. gal/day is expected.

1 **Wastewater Characteristics**

1.1. Wastewater Peak flow

The development served is a 4-bedroom single-family dwelling. The total plumbing fixture unit load in this residence is 21 based on a review of the building. This requires 11 lmp. gal/day be added to the base peak daily flow. Fixture unit load is as follows:

o Main bath = 6 fixture units

- o Bathroom with shower off master bedroom = 6 fixture units
- o Kitchen sink = 1.5 fixture units
- Laundry stand pipe = 1.5 fixture units
- Bathroom in basement = 6 fixture units

No high-volume plumbing fixtures were identified in the review of this development.

Total peak daily flo	ow used in the design is:	461 lmp. gal/day
Base flow :	450 lmp. gal	
Additional flow :	11 lmp. gal	

1.2. Wastewater Strength

Characteristics of the development were considered to assess sewage strength. No garbage grinders or other characteristics were identified that would cause typical wastewater strength to be exceeded.

Projected wastewater strength for the design is: TSS 220 mg/L Oil and Grease 50 mg/L	D : (]	BOD 220 mg/L
design is: Oil and Grease 50 mg/L	-	TSS 220 mg/L
	design is:	Oil and Grease 50 mg/L

1.3. Wastewater Flow Variation Considerations

The characteristics of this development indicate wastewater flow volumes will not vary substantially during the day or from day to day. No flow variation management is needed.

2 Site Evaluation Findings

2.1 Site Evaluation

The lot is 4 hectares (9.88 acres) in area. The dimensions of the property are shown in the drawing attached in Appendix A. The adjacent property is undeveloped farm land.

The proposed site has been reviewed as to consider the restrictions set out in Section 8.6.2.2 for prohibited open discharge installations. It has been confirmed that the number of subdivided parcels does not exceed 4, excluding the remnant parcel, as set out in the SOP.

The property has a 2% slope toward the north property line. Line locates confirmed there are existing utilities in along the north property line and an easement is in place.

The site evaluation assessed the area within in a 100 m (330 ft) radius of all components of the system design. No water courses or other setback constraints were noted. Pertinent features identified during the site review and the required setback distances are noted on the site plan in Appendix A.

2.2 Soils Evaluation

Two soil excavations were investigated on this site. Test Pit 1 is located at the proposed location of the open discharge outlet. The excavation for the basement was the second soil profile investigated. As these soil profiles show little variability they are adequate for design purposes. The location of test pit 1 is shown on the site plan in Appendix A. Soil profile descriptions are attached in Appendix B.

The area selected for the system must be kept clear of any utilities to be installed and no disturbance of the soil in that area can occur.

3 Key Soil Characteristics

3.1. Design Soil Conditions

- O Redoximorphic features (mottling/gleying) that indicate saturated soil are not present to a depth of 6 feet below surface.
- To a depth of 5 feet the dominate soil is a fine sandy loam with blocky grade 2 structure.

3.2. Limiting Soil Condition

No limiting condition encountered.

3.3. Effluent Linear Loading Rate Design Consideration

The open discharge system design considered the 2% ground slope. Landscaping at the point of discharge will be done to encourage spreading of the effluent.

4 Initial Treatment Component Design Details

Details of the initial treatment components required for this design are attached in Appendix C.

4.1 Septic Tank and Dose Tank

4.1.1 Septic Tank

The working capacity of the septic tank specified for this design is 1218 Imperial gallons. Specifications for the Model ST 1218 Septic Tank used in this design are shown in Appendix C.

The minimum working capacity required for this development is 951 lmp. gallons based on Table 4.2.2.2 of the 2009 SOP for a 4 bedroom house (940 lmp. gal/day plus the additional flow of 11 lmp. gal.)

Burial depth of the septic tank at finished grading will be 4ft 6 inches above the top of the tank. This tank is rated for a maximum burial depth of 9 ft.10 inches. Insulation of the tank is not required as the burial depth exceeds 4 feet.

4.1.2 Dose Tank

The dose chamber is integral to the septic tank. It has a total capacity of 670 Imp. gal. This is sufficient capacity to deliver the 111 Imp. gal required for each dose of effluent. It also provides 220 Imp. gal emergency storage above the high effluent alarm setting. Specifications are shown in Appendix C.

4.1.3 High Liquid Level Alarm

An Alarm Tech Inc JB Series 1000T high level alarm is specified for this system. It shall be set to activate at 30.5 inches above the floor of the dose tank.

4.1.4 Effluent Filter

An inline 2 inch diameter Sim/Tech[©] model STF-100 effluent filter having an effective opening of less than 3.2 mm (1/8") is used. It creates a head loss of 0.5 feet at its rated flow of 80 lmp. gal/min. A 5.5 foot pressure head allowance has been included in the pump selection to allow for partially clogged conditions. A one year service interval is expected with typical flow volumes and wastewater characteristics.

5 Effluent Discharge Pipe Design Detail

5.1 Effluent Discharge Pipe

The open discharge delivery pressure piping design calculations are provided in detail in Appendix E. The open discharge system schematic drawing is included in Appendix D.

Pressure head loss due to friction

The friction loss through the 290 feet of piping and filter at the flow of 13 lmp. gal/min is 12 feet of head pressure.

Pressure head to meet vertical lift requirements include:

- Lift distance of effluent from the low effluent level in the tank to the end of the open discharge pipe is 11feet.
- The design pressure head at end of open discharge pipe is 2 feet.

Vertical lift and friction loss results in a total pressure head requirement of 25 ft.

Pump specifications:

Demands for this pressure effluent line are 13 lmp. gal/min (15 U.S. gal/min) at 25 feet of pressure head.

A Myers model ME3F effluent pump (1/3 hp) is specified for this system. The pump specifications with the effluent distribution system demands plotted on the pump curve are included in Appendix C.

5.2 Effluent Dosing Volume and Control settings.

The volume of effluent discharged in a single dose event will be approximately 20% of the peak flow which is 92 gallons.

Liquid volume in 100 feet of 1 1/4 inch polyethylene pipe = 6.48 gallons.

For 290 feet of pipe the volume is 19 lmp. gallons

Total dose volume between on and off float settings =

92 Imp. gallons + 19 Imp. gallons = 111 Imp. gallons.

Total individual dose volume determining float settings is 111 lmp. gal in order to deliver 92 gallons per dose to the end of the open discharge pipe.

Effluent Level Float Control Settings

The dose tank dimensions result in $1\overline{2}$ Imp. gallons per inch of depth. The float control elevations shall be set at:

- 9 inches between float off and on elevations [111 lmp. gal ÷12 lmp. gal/inch].
- Off: 19 inches off floor of dose tank
- On: 28 inches off floor of dose tank
- Alarm set at 1.5 inches above pump on elevation (29.5 inches off floor based on float elevations set out in this design).

Redundant off float control is not required by this design. No manual pump on switch is included in the system. The effluent level control floats will be attached to a 1 inch PVC pipe independent float mast that will withstand the dose tank environment.

5.3 Effluent Quality Sampling

Effluent samples can be taken from the effluent dose tank if required.

6 Initial operational set up parameters

The following activities need to be conducted to commission the system:

- Clean the septic tank of any construction debris and flush effluent delivery line.
- Confirm the residual 2 foot head is achieved and the discharge is effectively controlled and directed to prevent erosion.
- Confirm float levels are set to deliver the dose volume required by this design.

7 Operation and Maintenance Manual

The Owner's Manual detailing the design, operation, and maintenance of the installed system will be provided to the owner in accordance with Article 2.1.2.8 of the Standard of Practice.

Signature and closing by the designer/Installer.

Attachments: Appendix A - Site Information [Site Plan, Drawings, etc.]

Appendix B – Soil Information, Soil Profiles, Laboratory Soil Analysis, etc.

Appendix C - Specifications for System Components

Appendix D - Detailed System Schematics, Drawings and Worksheets

This design has been developed by (name of certified person and company name). This design meets the requirements of the Alberta Private Sewage Systems Standard of Practice 2009 unless specifically noted otherwise and in such case special approval is to be obtained prior to proceeding with installation of this design. (Carry on with any other qualifications or limitations that in your opinion as the designer/installer are needed.)

Appendix A – Site Information

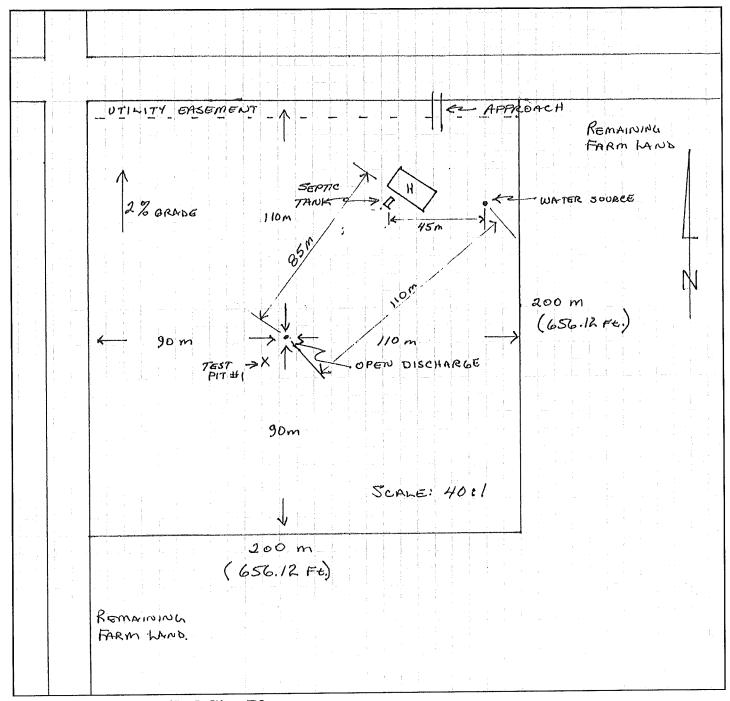


Figure A1 – Detailed Site Plan

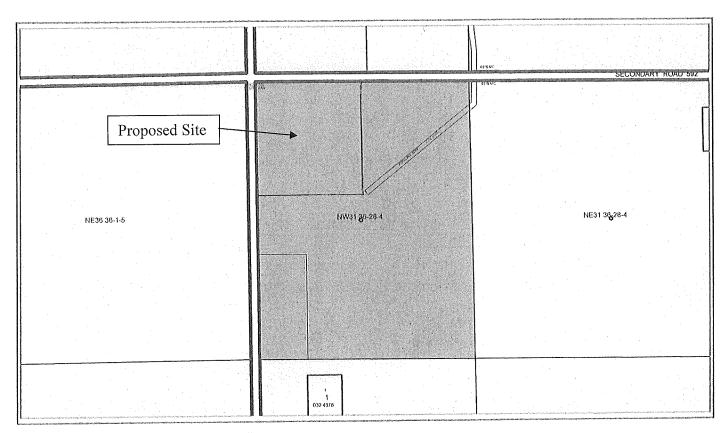


Figure A2 – Subdivision Plan

Appendix B - Alberta Private Sewage Treatment System Soil Profile Log Form

Smith Residence Soil Assessment	vce Soil Asse	ssment							
			Leg	Legal Land Location			Test I	Fest Pit GPS Coordinates	Т
LSD-1/4 Sec	Twp	Rg	Mer	Lot	Block	Plan	Easting	Northing	
NW 31	36	28	W4W	12	7	123450	65024	34535	
Investigation Date:	ite:	Vegeta	/egetation notes:	S:	Overall site slope	ite slope	2% at open a	2% at open discharge site.	
May 17th, 2011.		Praíríe	Praíríe grasses.		Slope po	Slope position of test pit:	upslope posít	upslope posítíon of property	
Test hole No.	Soil Subgroup	group	Pa	Parent Material	Drainage		Depth of Lab sample #1	Depth of Lab sample #2	
Test Pit #1						30-	30-36 in.		

A Surface to 24 Fine HT Dank brown. None. None. None. A Surface to 24 Fine Fine Moist to 26 Finality Sunday	Hori -zon	Depth (cm) (in)	Texture	Lab or HT	Colour	Gleying	Mottling	Structure	Grade	Consistence	Moisture	% Coarse Fragments
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		Ĺħ.	Sandy									
	-		(FSL)									
	А	24 to 60 in.	Fine	Ħ	Light brown.	None.	None.	Blocky	M	Fríable	Moíst to	5%
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(FSL) (FSL)			Loam	Lab								
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Comments (such as root depth and abundance or other pertinent observations): Roots extend to 5 feet (very fine at that depth) indicating no obvious limiting

characterístíc ín the soil.

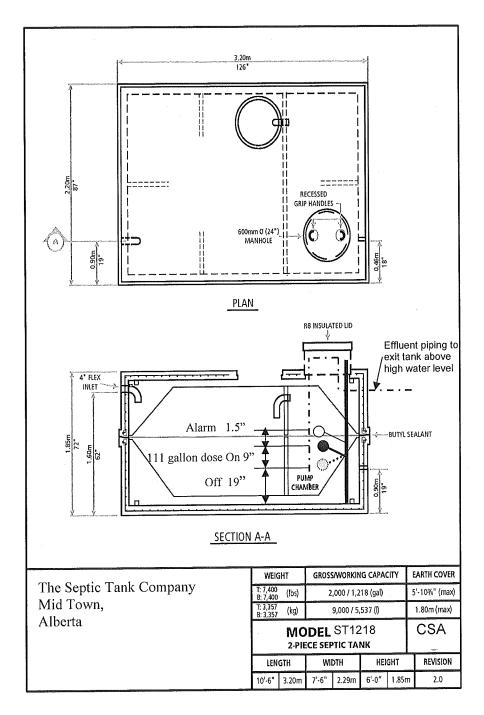
Appendix B - Alberta Private Sewage Treatment System Soil Profile Log Form

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22 to 63 in. Fine HT Light brown. None. None. Blocky and Loam (FSL) 63 to 84 in. Silt Loan HT Light brown. None. None. Blocky and Cast of the Sandy HT Light to Sandy HT Light to Sandy HT Light to Sandy Saturated Soil A+5 fet. 7 Soil Characteristics applied The Lab grain size analysis of the sand portion in the Fine Sandy loan soil system design effluent loading five grained. This is the key soil horizon the system design wust use alternated soil abundance or other pertinent observations): Five roots were observed to a depth moments (such as root depth and abundance or other pertinent observations): Five roots were observed to a depth		face to 22	Fine Sandy Loam (FSL)		<u> </u>	Dark brown.	None.	Nowe.	Granular	а	Fríable	Moíst	25%
e3 to 84 in.Silt LoamHTLight brownishNone.None.Prismati Prismati84 to 96 in.Sandly Clay (Sc)HTLight to Arrested ArresterAt \neq .5 ft is At \neq .5 ft is At \neq to \neq .5 ft At \neq to \neq .5 ft 		to 63 in.	Fine Sandy Loam (FSL)		rt nd ab	Líght brown.	None	Nowe.	Blocky	M	Fríable	Moíst to dry.	5 Je
84 to 96 in. Sandy HT Light to Atf.5ft is Atftof.5ft Massive clay (SC) dark grey. Saturated and gleyed. Arginet many and gleyed. Atftof.5ft Massive and gleyed. Atftof. Atftof. Atftof. Atftof. Massive and gleyed. Atftof. Massive and gleyed. Atftof. Atftof. Atftof. Atftof. Atftof. Massive and gleyed. Atftof. Atftof. Atftof. Atftof. Atftof. Massive and gleyed. Atftof. Atftof	<u> </u>	to 84 in.	Silt Loi (SIL)		-	Líght brownísh grey.	Nowe.	Nowe.	Prísmatíc	а	Slíghtly fríable.	Moist to dry.	84 89
aturated Soil 7-feet. Slightly undulating. The lab grain size analysis of the sand portion in the Fine Sandy loam soil. The lab grain size analysis of the sand portion in the Fine Sandy loam soil. The lab grain size analysis of the sand portion in the Fine Sandy loam soil. The lab grain size analysis of the sand portion in the Fine Sandy loam soil. The lab grain size analysis of the sand portion in the Fine Sandy loam soil. The lab grain size analysis of the sand portion in the Fine Sandy loam soil. The lab grain size analysis of the sand portion in the Fine Sandy loam soil. The lab grain size analysis of the sand portion in the Fine Sandy loam soil. The lab grain size analysis of the sand portion in the Fine Sandy loam soil. The lab grain size analysis of the sand portion in the Fine Sandy loam soil. The lab grain size analysis of the sand portion in the Fine Sandy loam soil. The lab grain size analysis of the sand portion in the Fine Sandy loam soil. The lab grain size analysis of the sand portion in the Fine Sandy loam soil. The lab grain size analysis of the sand portion in the Fine Sandy loam soil. The lab grain size analysis of the sand portion in the Fine Sandy loam soil. The lab grain size analysis of the sand portion in the Fine Sandy loam soil. The lab grain size and post of the sand portion in the Fine Sandy loam soil.		to 96 in.	Sandy Clay (s	(5)	+	Líght to dark grey.	At 7.5 ft is saturated and gleyed.	At F to F.5 ft many prominent distinct mottles	Massíve	0	Firm	Moist to wet.	<2%
Slightly undulating. The lab grain size analysis of the sand portion in the Fine Sandy loam soil. fine grained. This is the key soil horizon the system design must use. Atly overcast with moderate wind – no rain or other conditions that would impacinal abundance or other pertinent observations): Fine roots were observed to a depth	Depth to Gr	oundwater		7.5 feet.		Res	tricting Soil Layer	Characteristic	Sav	ndy clay uent mov	massíve struct ement.	ture restrícts d	ownward
The lab grain size analysis of the sand portion in the Fine Sandy loam soil fine grained. This is the key soil horizon the system design must use. httly overcast with moderate wind – no rain or other conditions that would impact and abundance or other pertinent observations): Fine roots were observed to a depth	Depth to Se	asonally Satura		7 feet.		Det	oth to restrictive So	oil Layer	7	eet.			
and wth	Site Topogr	aphy		Slightly	g unduli	"L T	oth to Highly Perm	eable Layer Limiting		encounte	ered in this soil	ls assessment	and design.
Weather Condition notes: Slightly overcast with moderate wind – no rain or other conditions that would impact soils assessment were encountered. Comments (such as root depth and abundance or other pertinent observations): Fine roots were observed to a depth of 5.5 ft.	Key Soil Cl	haracteristics a	applied loading	The lab	graín sí: íned. Th	ze analysís of i lís ís the key so	the sand portion il horizon the sy	in the Fine Sandy Isten design must	loam soil from	n 22 to 6.	3 inches detern	nined the san	d fraction is
Comments (such as root depth and abundance or other pertinent observations): Fine roots were observed to a depth of 5.5 ft.	Weather C	ondition notes	s: Slíghtl	y overcas	it with n	roderate wind -	- no raín or other	condítíons that we	ould impact so	ils assess	ment were enco	ountered.	
	Comments	(such as root	depth and	l abundar	ice or oth	her pertinent ob.	servations): Fine	roots were observed	to a depth of 2	5.5 ft.			

Insert lab analysis results of soil samples taken for determining soil texture!

Appendix C - Manufacturer's and Design Specifications for System Components

Septic Tank Specifications and Float Setting Details.



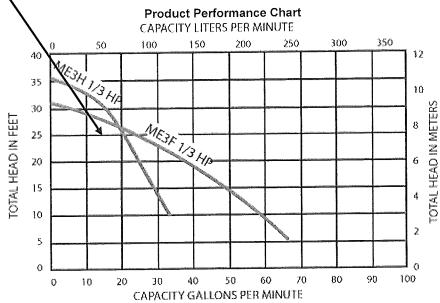
Pump Specifications

Myers Model ME3F Selected

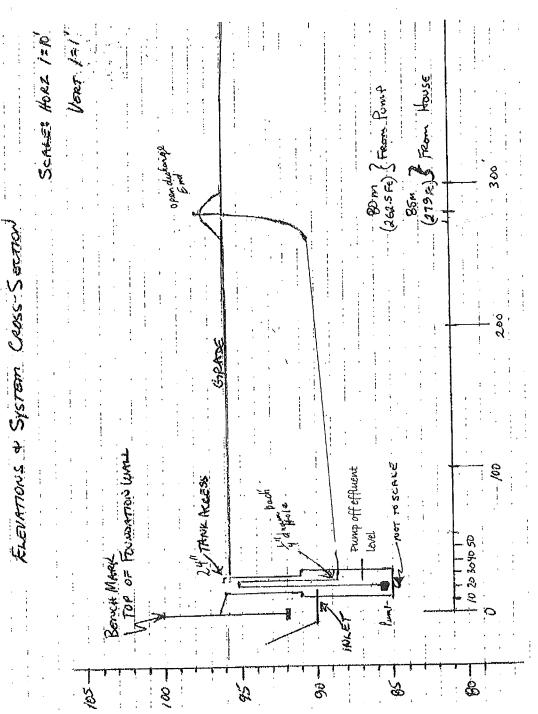
Product Capabilities

Capacities:	ME3H ME3F	36 GPM 66 GPM	136 LPM 249 LPM		
Shut-Off Head:	ME3H ME3F	35 ft. 31 ft.	10.7 m 9.5 m		
Max. Spherical Solid	s:	3/4 in.	19 mm		
Liquids Handling:		domestic effluer	nt and drain water		
Intermittent Liquid T	emp.:	up to 140°F	up to 60°C		
Motor Electrical Data	а:	shaded po 115V, 12A	1550 RPM, ble, oil-filled, A, 1Ø, 60Hz; A, 1Ø, 60Hz		
Housing:		heavy	cast iron		
Acceptable pH Rang	je:	6-9			
Specific Gravity:		.9–1.1			
Viscosity:		28–35 SSU			
Discharge, NPT:		1-1/2 in.	38.1 mm		
Min. Sump Diameter:	Simplex Duplex	24 in. 36 in.	61 cm 91.4 cm		
Power Cord:		20 in., 1	6/3, SJTW		

Smith residence system demand: 13 imp gal/min. (15 US gal/min) at 25 foot pressure head.







Sample doc only, representation of trade names does not indicate preference to products - Page 13

Pressure Distribution, Orifice, Pipe & Pump Sizing

This design worksheet was developed by Alberta Municipal Affairs and Alberta Onsite Wastewater Management Association.

The completed installation is to comply with Alberta Private Sewage Standard of Practice 2009.

This worksheet is for use in Alberta to: size the orifices in distribution lateral pipes, size effluent delivery piping, and to calculate the required capacity and pressure head capability of the effluent pump.

It can be used for: calculating delivery of effluent to laterals in disposal fields, mounds and sand filters.

This worksheet does NOT consider all of the mandatory requirements of the Standard.

It is intended for use by persons having training in the private sewage discipline.

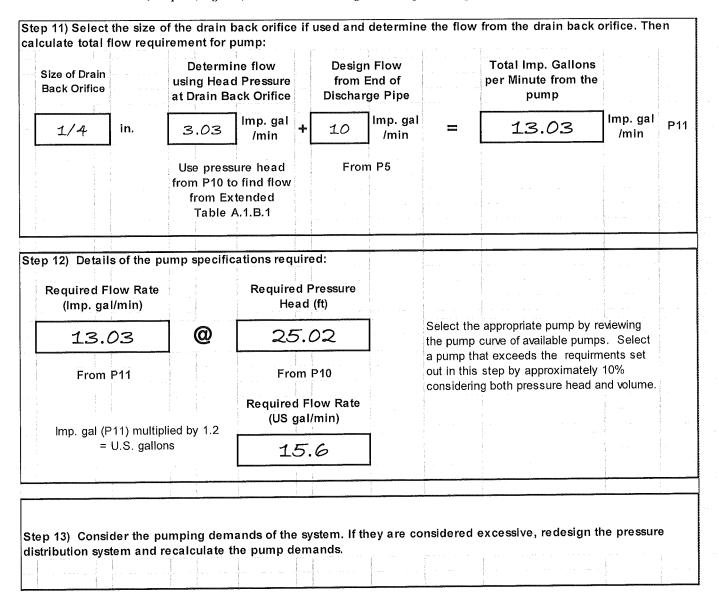
Note: Page numbers refer to the Private Sewage Systems Standard of Practice 2009.

Use only Imperial units of measurement throughout (feet, inches, Imperial gallons, etc...).

				1
Step 1) Select the pressure head	to be maintained at the ori	nces:		1
Minimum pressure at the orifice:	0.005 (1) (1.40)			
3/16" or less orifice = 5 ft. Minimu	ım - 2.6.2.5 (1), (p 48)			
larger than 3/16" orifice = 2 ft. Mil	nimum - 2.6.2.5 (1) (p 48)			
Design pre	ssure at Lateral Orifices ft.	2 ft abou	re pipe end #.	P1
	I was to desire if laterals are at diff.	arant alayations Differin	a elevations will result in a	
Note: worksheet will not provide an acdifferent pressure head and volume of controls.	dequate design if laterals are at dille Vischerge at the orifices in each lat	eren elevations. Dillerni eral Additional consider	rations must be made f	
different pressure nead and volume of the	discharge at the offices in each fac-	orar. Maarronar conc.acr		
Step 2) Select the size of orifice i	n the laterals:			
otop 2) dolloot tilo dizo di diliida				
		Orifice Diameter	in and in also a large in	P2
Minimum size: 2.6.1.5. (1)(e) p. 46	1/8"	selected	not applicable/na in.	Γ 2.
			A STATE OF THE PARTY OF THE PAR	
Alata Janaaraina ara laga likohi ta plu		† . I		
Note: larger sizes are less likely to plu	J.			
		:		:
Length of Distribution Lateral From system design drawings	Spacing of Orifices se design	lected for	Resulting number of orifices per lateral	
NA ft.	÷ na	ft. =	na	P3a
7001		_		_
Select a spacing of orifices to at	ain even distribution over the t	reatment area:		
Maximum spacings are determin				'
* 5 ft. Primary treated effluent: 2	6 1 5 (e) (nn. 46 - 47)			
* 3 ft. Secondary treated effluent	8 1 1 8 8 2 6 2 2 (c) (nn 98	8 47 - 48)		
		۵, ۱۱ ام)		
* 3 ft. On sandy textured soils: 8	5. 1. 1.0 (þ. 90)	1		
I na I x I	na =		na	P3b
		Total Nivos	ber of Orifices All Laterals	!
From P3a Nu	mber of Laterals	iotai ivum	per of Offices All Laterals	
If laterals are of differing lengths, calc	ulate each separately and add the r	number of orifices togethe	er.	

Step 4) Determine the mi Enter the system design in					erals are	of differing lengths, ea	ch lateral m	ust be
	<i>t</i>	C	onsidered s	separately.			ļ	
Orifice Diameter	L	ength of Distr	ibution La	iteral		Total Orifices Eac	n Lateral	
1.25	in.	n	Я	ft.		1		
From P2		From System D	esian Draw	⊥ vinas		From P3a		!
Use Table A.1.A. (pp 140 - 1-					ermine the i	minimum size of the distrib	oution lateral _l	pipe.
		Size		ution Latera From Table		na	in.	P4
Step 5) Determine the tot	al flow fron			•			-	
Total Number of Orifices in all laterals		Gal/min f Orifice a Pressure	t Head			Total flow from a orifices	II lateral	
1	x	10)	lmp. gal /min.	protes	10	lmp. gal /min.	P5
From P3b		From Tabl (pp 144			- -			
Step 6) Select the type a	nd size of e	ffluent delive	ry nine:					
Use Tables A1.C.1 to A1			Type of	pipe used nt delivery	Piŗ	e size selected		Appropriate and the second
in decision. A larger pipe loss.	will reduce p	pressure		thylene		1 1/4	inch - NPS	P6
Choose a friction loss fro	m Tables A1 lcted will affe	.C.1 to A1.C.4 ii ct the amount of	n between t friction loss	he bolded line s the pump m	es to ensu ust overco	re a flow velocity betwee me to deliver effluent.	en 2 to 5 feet	per
								:
Step 7) Calculate the equ	uivalent len	igth of pipe fo	r pressure	loss due to		alent Length of All		
Insert total from Worksh	neet "A" on la	ast page (p.5) of	this			Fittings 100	T ft.	P7
Pressure Distribution W				L.		٠٠٠٠		

Length of Piping (ft)		equivalent Length of Fi (ft)	ttings	Length	of Pipe for Friction Loss (ft)		
290	+	19.8	Name		310	·	P
ength from pump to end f open discharge piping.	The state of the s	Equivalent fitting length from P7 .	to become more face. The state of the state of	j.	etermine total pressure due to friction loss in		
					:		
9) Calculate the pressure	e head	loss in delivery pipe in	ncluding fit	tings:			:
Total Length of Pipe for Friction Loss	The second secon	Friction Loss per 100 feet of pipe		*** *** *** *** *** *** *** *** *** **	Delivery Piping Pressure Head Loss		† : :
310	X	2.11 ft	divide 100		6.54	ft.	. P
From P8							
con't forget to divide the ength by 100 feet to match ne factors in the tables.		Use Tables A1.C. On pp using flow volume from I					
						:	
10) 0 1 1 1 1 1 1 1 1 1 1		hand required at pur				: 	
o 10) Calculate the total p	ressure	e lleau required at puil	ib.			1	
Delivery piping pressure loss	and the second s	6.54	ft.	From P9			
		+	_				1
Lift distance of effluent from effluent tank level to open discharge pipe		11	ft.		from lowest effluent nk to elevation of open d	lischarge	point
	1	+	-	1		1	1.4
Design pressure at open discharge end		2	ft.	From P1			
		+	-				
Head loss allowed if an inline filter is used in pressure piping		5.48	ft.	A pressu	Pressure Loss Allowed re loss of 0.48ft acros until alarm goes off		ed
biocogio bibilià							
Total minimum pressure pump must provide a lmp. gal/min required	at	25.02	ft.	P10			



Worksheet ".	Appendix A" Determin	e Equivalen	t Length of Pipe due	to fittings	in piping system.	
Determine the	e equivalent length of pip	e to allow for t	friction loss due to fittin	ngs in the p	iping system:	
	Number of Fittings		Friction loss as per Table A.1.C.5 or 6		Total	
90° Elbows	3	X	3.8	Science Science	11.4	
				The state of the s	+	
45°Elbows		х		==		
					+	
Gate and Ball Valves		х		Name of the last o		
Officers (Fig. 2)					+	
Tee-on- Branch (TOB)		х				
To characteristic de la participa de la partic					+	1
Tee-on-Runs (TOR)		x		points busins		
: : :					+	
Male Iron pipe Adaptors	3	x	2.8	=	8.4	
(M/F Threade	ed Adaptors)				=	
Total Equivale	ent Length of pipe to allo ing system	w for	(Enter this total,	Box P7)	19.8	

Pressure Distribution, Orifice, Pipe & Pump Sizing

This design worksheet was developed by Alberta Municipal Affairs and Alberta Onsite Wastewater Management Association.

The completed installation is to comply with Alberta Private Sewage Standard of Practice 2009.

This worksheet is for use in Alberta to: size the orifices in distribution lateral pipes, size effluent delivery piping, and to calculate the required capacity and pressure head capability of the effluent pump.

It can be used for: calculating delivery of effluent to laterals in disposal fields, mounds and sand filters.

This worksheet does NOT consider all of the mandatory requirements of the Standard. It is intended for use by persons having training in the private sewage discipline.

Note: Page numbers refer to the Private Sewage Systems Standard of Practice 2009.

Use only Imperial units of measurement throughout (feet, inches, Imperial gallons, etc...).

					Parameter Committee Committee and the alleger
Step 1) Select the pressure head to be	e maintained at the orif	ices:			
Minimum pressure at the orifice:					
3/16" or less orifice = 5 ft. Minimum -	2.6.2.5 (1). (p.48)				
larger than 3/16" orifice = 2 ft. Minimu					
	(.) (p)				
Design	pressure at lateral orifice	es		ft.	P1
_					
Note: worksheet will not provide an adequate	e design if laterals are at differ	ent elevations. Differing elevat	ions will result in a different		
pressure head and volume of discharge at the	orifices in each lateral. Additi	ional considerations must be m	ade for laterals at differing		
elevations.					
					. Tarabar alambar yan Tara
Step 2) Select the size of orifice in the	laterals:				enconstruit en
otop 2) delect the size of office in the	ideorais,				
		Ouldier Dienerten			
Minimum size: 2.6.1.5. (1)(e) p. 46	1/8"	Orifice Diameter		in.	P2
\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \		selected			
Note: larger sizes are less likely to plug.					
					an 1000 disebit na ellaren narradon
					and the second
Ston 3) Salact the enacing of orificae	and determine the nun	nhar of arificas to be in	stalled in distribution la	torales	
Step. 3) Select the spacing of orifices	and determine the nun	nber of orifices to be in	stalled in distribution la	terals:	
Length of Distribution Lateral	Spacing of Orifices		Resulting number of		:
Length of Distribution Lateral	Spacing of Orifices		Resulting number of		:
Length of Distribution Lateral From system design drawings	Spacing of Orifices	selected for	Resulting number of		Do
Length of Distribution Lateral	Spacing of Orifices		Resulting number of		P3a
Length of Distribution Lateral From system design drawings	Spacing of Orifices	selected for	Resulting number of		P3a
Length of Distribution Lateral From system design drawings	Spacing of Orifices	selected for	Resulting number of		P3a
Length of Distribution Lateral From system design drawings ft. ÷	Spacing of Orifices design	selected for	Resulting number of		P3a
Length of Distribution Lateral From system design drawings ft. ÷ Select a spacing of orifices to attain e	Spacing of Orifices design	selected for	Resulting number of		P3a
Length of Distribution Lateral From system design drawings ft. ÷ Select a spacing of orifices to attain e Maximum spacings are determined for	Spacing of Orifices design ven distribution over the or :	selected for	Resulting number of		P3a
Length of Distribution Lateral From system design drawings ft. ÷ Select a spacing of orifices to attain e Maximum spacings are determined for * 5 ft. Primary treated effluent: 2.6.1.5	Spacing of Orifices design ven distribution over the or: 5 (e) (pp. 46 - 47)	selected for ft. = treatment area:	Resulting number of		P3a
Length of Distribution Lateral From system design drawings ft. ÷ Select a spacing of orifices to attain e Maximum spacings are determined for * 5 ft. Primary treated effluent: 2.6.1.8 * 3 ft. Secondary treated effluent: 8.1	Spacing of Orifices design ven distribution over the or: 5 (e) (pp. 46 - 47) 1.8 & 2.6.2.2 (c) (pp 98	selected for ft. = treatment area:	Resulting number of		P3a
Length of Distribution Lateral From system design drawings ft. ÷ Select a spacing of orifices to attain e Maximum spacings are determined for * 5 ft. Primary treated effluent: 2.6.1.5	Spacing of Orifices design ven distribution over the or: 5 (e) (pp. 46 - 47) 1.8 & 2.6.2.2 (c) (pp 98	selected for ft. = treatment area:	Resulting number of		P3a
Length of Distribution Lateral From system design drawings ft. ÷ Select a spacing of orifices to attain e Maximum spacings are determined for * 5 ft. Primary treated effluent: 2.6.1.8 * 3 ft. Secondary treated effluent: 8.1	Spacing of Orifices design ven distribution over the or: 5 (e) (pp. 46 - 47) 1.8 & 2.6.2.2 (c) (pp 98	selected for ft. = treatment area:	Resulting number of		P3a
Length of Distribution Lateral From system design drawings ft. ÷ Select a spacing of orifices to attain e Maximum spacings are determined for * 5 ft. Primary treated effluent: 2.6.1.8 * 3 ft. Secondary treated effluent: 8.1 * 3 ft. On sandy textured soils: 8.1.1.8	Spacing of Orifices design ven distribution over the or: 5 (e) (pp. 46 - 47) 1.8 & 2.6.2.2 (c) (pp 98	selected for ft. = treatment area:	Resulting number of		
Length of Distribution Lateral From system design drawings ft. ÷ Select a spacing of orifices to attain e Maximum spacings are determined for * 5 ft. Primary treated effluent: 2.6.1.8 * 3 ft. Secondary treated effluent: 8.1	Spacing of Orifices design ven distribution over the or: 5 (e) (pp. 46 - 47) 1.8 & 2.6.2.2 (c) (pp 98	selected for ft. = treatment area:	Resulting number of		P3a P3b
Length of Distribution Lateral From system design drawings ft. : Select a spacing of orifices to attain e Maximum spacings are determined fo * 5 ft. Primary treated effluent: 2.6.1.8 * 3 ft. Secondary treated effluent: 8.1 * 3 ft. On sandy textured soils: 8.1.1.8	Spacing of Orifices design ven distribution over the or: 5 (e) (pp. 46 - 47) 1.8 & 2.6.2.2 (c) (pp 98	selected for ft. = treatment area: & 47 - 48)	Resulting number of per lateral	orifices	
Length of Distribution Lateral From system design drawings ft. ÷ Select a spacing of orifices to attain e Maximum spacings are determined for * 5 ft. Primary treated effluent: 2.6.1.8 * 3 ft. Secondary treated effluent: 8.1 * 3 ft. On sandy textured soils: 8.1.1.8	Spacing of Orifices design ven distribution over the or: 5 (e) (pp. 46 - 47) .1.8 & 2.6.2.2 (c) (pp 98 8 (p. 98)	selected for ft. = treatment area: & 47 - 48)	Resulting number of	orifices	
Length of Distribution Lateral From system design drawings ft. : Select a spacing of orifices to attain e Maximum spacings are determined fo * 5 ft. Primary treated effluent: 2.6.1.8 * 3 ft. Secondary treated effluent: 8.1 * 3 ft. On sandy textured soils: 8.1.1.8	Spacing of Orifices design ven distribution over the or: 5 (e) (pp. 46 - 47) .1.8 & 2.6.2.2 (c) (pp 98 g (p. 98)	ft. = treatment area: & 47 - 48) Total Number	Resulting number of per lateral	orifices	

Revision Date: May 17, 2010 HO 112 - 02

Enter the system design information into the 3 boxes below. If distribution laterals are of differing lengths, each lateral must be considered separately. Orifice Diameter Length of Distribution Lateral in. From P2 From System Design Drawings Use Table A.1.A. (pp 140 - 143) when applying the information entered in this step to determine the minimum size of the distribution lateral pipe. Size of Distribution Lateral Pipe From Table A.1.A. In. P4 Step 5) Determine the total flow from all orifices: Total Number of Orifices in all laterals At Head Pressure Selected Total flow from all lateral orifices Imp. gal /min. From P3b From Table A.1.B. (pp 144 & 145)
Considered separately. Orifice Diameter in. From P2 Use Table A.1.A. (pp 140 - 143) when applying the information entered in this step to determine the minimum size of the distribution lateral pipe. Size of Distribution Lateral Pipe From Table A.1.A. Step 5) Determine the total flow from all orifices: Total Number of Orifices in all laterals A Gal/min for each Orifice at Head Pressure Selected Total flow from all lateral orifices Imp. gal /min. From P3b From Table A.1.B. (pp 144 & 145)
Orifice Diameter In. From P2 From System Design Drawings From P3a Use Table A.1.A. (pp 140 - 143) when applying the information entered in this step to determine the minimum size of the distribution lateral pipe. Size of Distribution Lateral Pipe From Table A.1.A. Step 5) Determine the total flow from all orifices: Total Number of Orifices in all laterals A Gal/min for each Orifice at Head Pressure Selected Imp. gal /min. From P3b From Table A.1.B. (pp 144 & 145)
in. From P2 Use Table A.1.A. (pp 140 - 143) when applying the information entered in this step to determine the minimum size of the distribution lateral pipe. Size of Distribution Lateral Pipe From Table A.1.A. Step 5) Determine the total flow from all orifices: Total Number of Orifices in all laterals X Gal/min for each Orifice At Head Pressure Selected Imp. gal /min. From P3b From Table A.1.B. (pp 144 & 145)
in. From P2 Use Table A.1.A. (pp 140 - 143) when applying the information entered in this step to determine the minimum size of the distribution lateral pipe. Size of Distribution Lateral Pipe From Table A.1.A. in. P2 Step 5) Determine the total flow from all orifices: Total Number of Orifices in all laterals A Head Pressure Selected Imp. gal /min. From P3b From Table A.1.B. (pp 144 & 145)
Use Table A.1.A. (pp 140 - 143) when applying the information entered in this step to determine the minimum size of the distribution lateral pipe. Size of Distribution Lateral Pipe From Table A.1.A. In. P2 Step 5) Determine the total flow from all orifices: Total Number of Orifices in all laterals at Head Pressure Selected orifices Imp. gal /min. From P3b From Table A.1.B. (pp 144 & 145)
Use Table A.1.A. (pp 140 - 143) when applying the information entered in this step to determine the minimum size of the distribution lateral pipe. Size of Distribution Lateral Pipe From Table A.1.A. In. Particle Step 5) Determine the total flow from all orifices: Total Number of Orifices in all laterals at Head Pressure Selected orifices X Imp. gal /min. From P3b From Table A.1.B. (pp 144 & 145)
From Table A.1.A. Step 5) Determine the total flow from all orifices: Total Number of Orifices in all laterals X Gal/min for each Orifice at Head Pressure Selected Orifices Imp. gal /min. From P3b From Table A.1.B. (pp 144 & 145)
From Table A.1.A. Step 5) Determine the total flow from all orifices: Total Number of Orifices in all laterals X Gal/min for each Orifice at Head Pressure Selected Orifices Imp. gal /min. From P3b From Table A.1.B. (pp 144 & 145)
Step 5) Determine the total flow from all orifices: Total Number of Orifices in all laterals X Gal/min for each Orifice at Head Pressure Selected Imp. gal /min. From P3b From Table A.1.B. (pp 144 & 145)
Total Number of Orifices in all laterals X Gal/min for each Orifice at Head Pressure Selected Imp. gal /min. From P3b From Table A.1.B. (pp 144 & 145)
Total Number of Orifices in all laterals X Gal/min for each Orifice at Head Pressure Selected Imp. gal /min. From P3b From Table A.1.B. (pp 144 & 145)
Orifices in all laterals At Head Pressure Selected Imp. gal /min. From P3b From Table A.1.B. (pp 144 & 145)
Mp. gal Imp. gal
From P3b From Table A.1.B. (pp 144 & 145)
From P3b From Table A.1.B. (pp 144 & 145)
(pp 144 & 145)
(pp 144 & 145)
Step 6) Select the type and size of effluent delivery pipe:
Type of pipe used
for effluent delivery Pipe size selected
Use Tables A.1.C.1 to A.1.C.4 (pp 146 - 149) to aid in decision. A larger pipe will reduce pressure loss.
- IN O
Choose a friction loss from Tables A.1.C.1 to A.1.C.4 in between the bolded lines to ensure a flow velocity between 2 to 5 feet per second. T
pipe size selcted will affect the amount of friction loss the pump must overcome to deliver effluent.
Step 7) Calculate the equivalent length of pipe for pressure loss due to fittings:
Equivalent Length of All Fittings
Insert total from Worksheet "A" on last page (p.5) of this Pressure
Distribution Worksheet It.

Revision Date: May 17, 2010 HO 112 - 02

Step 8) Calculate the equival	ent lengf	th of pipe from pump to th	ne farthes	st end of header of distribution laterals for p	pressure
loss: Length of Piping		Equivalent Length of Fitti		Length of Pipe for Friction Loss	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
(ft)	+	(ft)		(ft)	P8
Length from pump to farthest end of distribution header supplying laterals.		Equivalent fitting length from P7.		Used to determine total pressure head loss due to friction loss in piping.	
Step 9) Calculate the pressu	re head I	loss in delivery pipe inclu	ding fittir	ngs:	
Total Length of Pipe for Friction Loss		Friction Loss per 100 feet of pipe	~ 1	Delivery Piping Pressure Head Loss	
Divide by 100 ft.	x		ft.	= ft.	P9
From P8		- · · · · · · · · · · · · · · · · · · ·			
Don't forget to divide the length by 100 feet to match the factors in the tables.		Use Tables A.1.C. On pp 14 using flow volume from P5.			
Step 10) Calculate the total p	ressure	head required at pump:			
Delivery piping pressure loss			ft.	From P9	
Lift distance of effluent from effluent level in tank to orifices		+	ft.	Measure from lowest effluent level in tank to elevation of orifices.	
Design pressure at orifices		+	ft.	From P1	
Head loss allowed if an inline filter is used in pressure piping		+	ft.	Explain Pressure Loss Allowed if Applied	
Add 1 ft to allow for pressure loss along the		+	ft.		

P10

ft.

Total minimum pressure head

pump must provide at Imp. gal/min required to supply orifices

distribution lateral

Step 11) Select the size of total flow requirement for	the drain back orifice if us pump:	ed and determine the	flow froi	n the drain back orifice.	Then calc	ulate
Size of Drain Back Orifice	Determine flow using Head Pressure at Drain Back Orifice	Flow from all lateral orifices		Total Imp. Gallons per Minute from the pump		
in.	Imp. gal /min	lmp. gal /min	and the second		lmp. gal /min	P11
	Use pressure head from P10 to find flow from Extended Table A.1.B.1	From P5				

Required Flow Rate (Imp. gal/min)	Required Pressure Head (ft)	
(9	Select the appropriate pump by reviewing the pump curve of available pumps. Select a
From P11	From P10	pump that exceeds the requirments set out in this step by approximately 10% considering both pressure head and volume.
Imp. gal (P11) multiplied by 1	Required Flow Rate (US gal/min)	considering both pressure nead and volume.
= U.S. gallons		

Step 13) Consider the pumping demands of the system. If they are considered excessive, redesign the pressure distribution system and recalculate the pump demands.

Worksheet "Appendix A" Determine Equivalent Length of Pipe due to fittings in piping system.						
Determine the	equivalent length of pipe	to allow for f	riction loss due to fitting	s in the pip	oing system:	
	Number of Fittings		Friction loss as per Table A.1.C.5 or 6 (p. 150)		Total	_
90° Elbows		X		12000 12000		
					+	•
45°Elbows		X		income income		
,					+	•
Gate and Ball Valves		Х		Marinesi Marinesi		
					+	
Tee-on- Branch (TOB)		Х		terone terone		
`					+	
Tee-on-Runs (TOR)		X		1000 S		
					+	
Male Iron pipe Adaptors		x				
(M/F Threaded	d Adaptors)					
					1000 1000	
Total Equivale in piping syste	nt Length of pipe to allow f m	or fittings	(Enter this total, E	Box P7)		

Alberta Private Sewage Treatment System Soil Protile Log Form Vegetation notes: Key Soil Characteristics applied to system design effluent loading Comments: such as root depth and abundance or other pertinent observations: Site Topography Depth to Seasonally Saturated Soil Depth to Groundwater Owner Name or Job ID. Weather Condition notes: Hori-zon Test hole No. LSD-1/4 (cm) (in) Depth Sec Soil Subgroup Twp Texture Rg Lab or HT Legal Land Location Mer Colour Parent Material Lot Depth to Highly Permeable Layer Limiting Design Depth to restrictive Soil Layer Restricting Soil Layer Characteristic Gleying Block Slope position of test pit: Overall site slope % Drainage Mottling Plan Structure Depth of Lab sample #1 Grade Easting Consistence Test Pit GPS Coordinates Depth of Lab sample #2 Moisture Northing Fragments % Coarse

Alberta Private Sewage Treatment System Soil Profile Log Form Owner Name or Job ID.

Vegetation notes: Depth to Seasonally Saturated Soil Comments: such as root depth and abundance or other pertinent observations: system design effluent loading Key Soil Characteristics applied to Site Topography Depth to Groundwater Weather Condition notes: Hori-zon Test hole No. LSD-1/4 (cm) (in) Depth Sec Soil Subgroup Twp Texture Rg Lab or HT Legal Land Location Mer Colour Parent Material Lot Depth to Highly Permeable Layer Limiting Design Depth to restrictive Soil Layer Restricting Soil Layer Characteristic Gleying Block Overall site slope % Slope position of test pit: Drainage Mottling Plan Structure Depth of Lab sample #1 Grade Easting Consistence Test Pit GPS Coordinates Depth of Lab sample #2 Moisture Northing Fragments % Coarse

Onsite Sewage System Site Evaluation Lot Diagram Field Sketch and Notes Lot or Legal Description: Project Name: Show the proposed location of the onsite sewage system and the following items indicating their distances from the proposed system: trees floodplains wells water sources surface water bedrock outcrops buildings property lines easement lines ditches or interceptors banks or steep slopes fills driveways existing sewage systems underground utilities soil test pit borehole locations Test Pit P1 borehole slope direction drainage course BH 1

Comments:

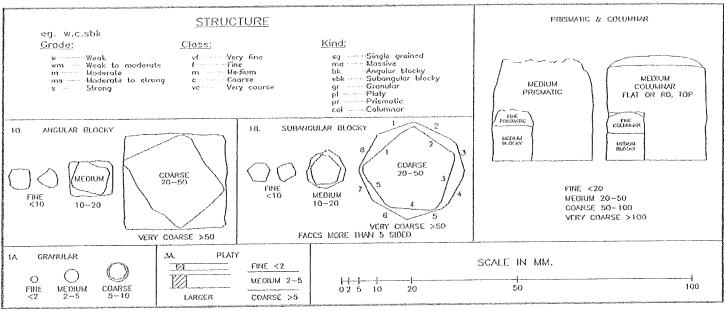
Property line GPS coordinates:

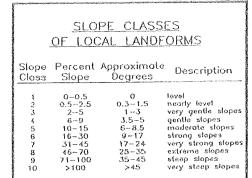
GPS coordinates of well:

GPS coordinate of tank:

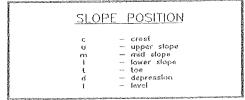
GPS coordinates of soil treatment component corners:

Figure 4: Diagrammatic representation of soil structure





	SURFACE	STONIN	<u>ESS</u>
		Surface Area	Distance Apart (cm)
50 51 52 53 54 55	non-stony slightly stony moderately stony very stony exceedingly stony exceesively stony	<0.01% 0.01-0.1% 0.1-3% 3-15% 16-50% 50%	>30 10-30 2-10 1-2 0,1-5 0,1



<u>Df</u>	11A5	<u>IAGE</u>
VR	-	very rapidly
R		rapidly
V¥	-	welf
M		moderately well
1		imperfectly
P	_	pourly
VP	-	very poorly

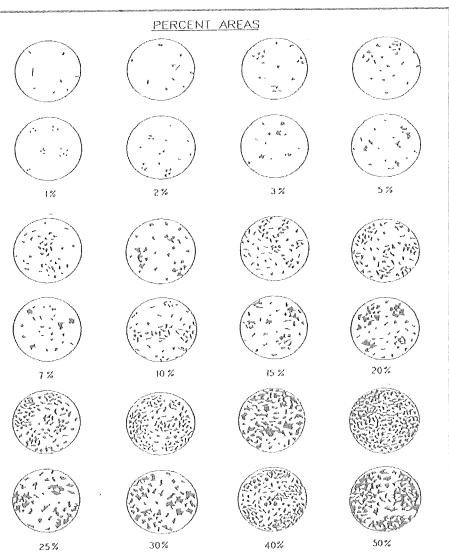


Table 10. Types, kinds and classes of soil structure.

Type Blocklike - soil particles arranged around a point and bounded by flat or rounded surfaces BK	Kind (Kind Code) Angular blocky (ABK) peds bounded by flattened, rectangular faces intersecting at relatively sharp angles	Structure Class and Code VF: very fine angular blocky F: fine angular blocky M: medium angular blocky C: coarse angular blocky VC: very coarse angular blocky	Size ¹ (mm) <5 5-10 10-20 20-50 >50
	Subangular blocky (SBK): peds bounded by slightly rounded, subrectangular faces with vertices ² of their intersections mostly subrounded	 VF: very fine subangular blocky F: fine subangular blocky M: medium subangular blocky C: coarse subangular blocky VC: very coarse subangular blocky 	<5 5-10 10-20 20-50 >50
	Granular (GR): spheroidal peds bounded by curved or very irregular faces that do not adjoin those of adjacent peds	 VF: very fine granular F: fine granular M: medium granular C: coarse granular VC: very coarse granular 	<1 1-2 2-5 5-10 >10
Platelike: soil particles arranged around a horizontal plane and generally bounded by relatively flat horizontal surfaces	Platy (PL): peds flat or platelike; horizontal planes more or less well developed	VF: very fine platyF: fine platyM: medium platyC: coarse platyVC: very coarse platy	<1 1-2 2-5 5-10 >10
PL Prismlike: soil particles arranged around a vertical axis and bounded by relatively flat vertical surfaces.	Prismatic (PR): vertical faces of peds well defined and vertices ² angular (edges sharp); prism tops essentially flat	 VF: very fine prismatic F: fine prismatic M: medium prismatic C: coarse prismatic VC: very coarse prismatic 	<10 10-20 20-50 50-100 >100
PR	Columnar (COL): vertical edges near top of columns not sharp (vertices ² subrounded); column tops flat, rounded, or irregular	 VF: very fine columnar F: fine columnar M: medium columnar C: coarse columnar VC: very coarse prismatic 	<10 10-20 20-50 50-100 >100
Structureless: no observable aggregation of primary	Single grained (SGR):	Loose, incoherent mass of indiv particles, as in sands	idual primary
particles or no definite orderly arrangement around natural lines of weakness MA	Massive (MA):	amorphous; a coherent mass showing any distinct arrangement of soil part into clusters of particles; not peds	no evidence of icles; separates

Cloddy (CDY): not a structure; used to indicate the condition of some ploughed surface, grade, class, and shape too varied to be described in standard terms.

Consistence – moist	soil
• Loose:	No intact sample can be obtained.
• Friable:	Structure breaks down with slight force between the fingers.
• Firm:	Structure breaks down with moderate force between the fingers.
Extremely firm:	Structure breaks down with moderate force between the hands or
·	slight foot pressure.
• Rigid:	Structure breaks down only with foot pressure.

The size limits refer to measurements in the smallest dimension of platy, prismatic, and columnar peds and to the largest of the nearly equal dimensions of blocky and granular peds.
 Definition of vertex (plural, vertices): the intersection of two planes of a geometrical figure.

Structure Grade Descriptions

Code		Structure Grade Definition			
0	Massive /or single grained used to describe sands	This describes a soil that has no developed structure. There is no aggregation of primary particles or no definite orderly arrangement around natural lines of weakness.			
1	Weak	Peds are either indistinct and barely evident in place, or observable in place but incompletely separated from adjacent peds. When disturbed, the soil material separates into a mixture of only a few entire peds, many broken peds and much unaggregated material.			
2	Moderate	Peds are moderately durable, and are evident but not distinct in the undisturbed soil. When disturbed, the soil material parts into a mixture of many well formed, entire peds, some broken peds, and little unaggregated material. The peds may be handled without breaking and they part from adjoining peds to reveal nearly entire surfaces which have properties distinct from those caused by fracturing.			
3	Strong	Peds are durable and evident in the undisturbed soil, adhere weakly to one another, withstand displacement and separate cleanly when the soil is disturbed. When removed, the soil material separates mainly into entire peds. Surfaces of unbroken peds have distinctive properties, compared to surfaces that result from fracturing.			

Mottling Descriptions

Parameter	Code	Description
Abundance	Few	<2% of the exposed surface
	Common	2-20% of the exposed surface
	Many	>20% of the exposed surface
Size	Fine	< 5 mm
	Medium	5-15 mm
	Coarse	>15 mm
Contrast	Faint	Evident only on close examination. Faint mottle commonly have the same hue as the colour to which they are compared and differ by no more than 1 unit of chroma or 2 units of value. Some faint mottles of similar but low chroma and value can differ by 2.5 units of hue.
	Distinct	Readily seen, but contrast only moderately with the colour to which they are compared. Distinct mottle commonly have the same hue as the colour to which they are compared, but differ by 2 to 4 units of chroma or 3 to 4 units of value; or differ from the colour to which they are compared by 2.5 units of hue but by no ore than 1 units of chroma or 2 units of value.
	Prominent	Contrast strongly with the colour to which they are compared. Prominent mottles are commonly the most obvious colour feature in a soil. Prominent mottles that have medium chroma and value commonly differ from the colour to which they are compared by at least 5 unit of hue if chroma and value are the same; or at least 1 un of chroma or 2 units of value if hue differs by 2.5 units.

